## ELEMEN

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# 7th INTERNATIONAL FOUNDRY CONGRESS & EXHIBITION (IFCE-2018)

14th-15th November 2018, Pearl Continental Hotel, Lahore

















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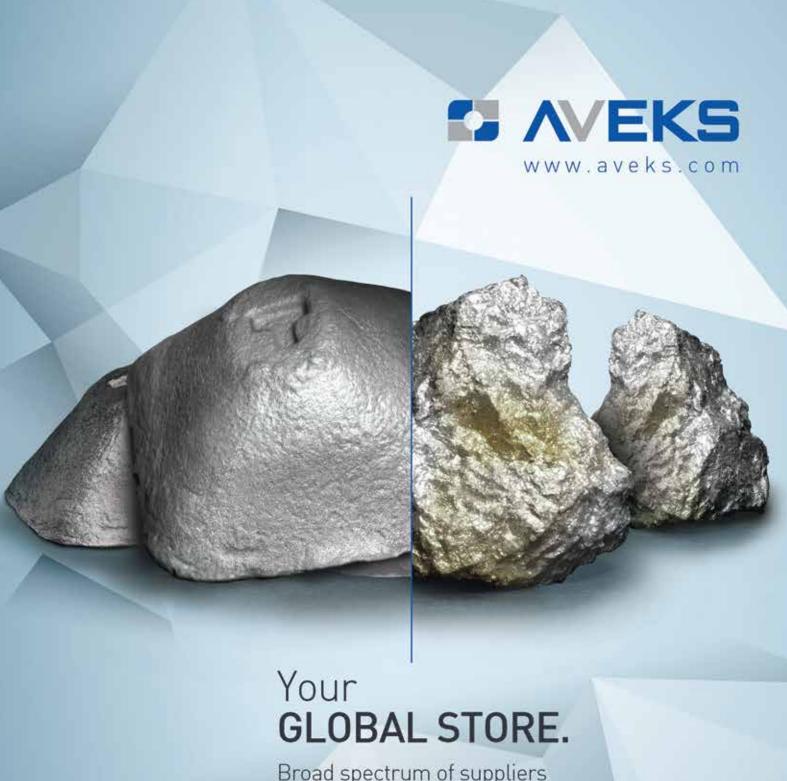




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## PRESIDENT MESSAGE

Pakistan Foundry Association (PFA) will organize International Foundry Congress & Exhibition (IFCE-2018) on 13th-15th November, 2018 at Pearl Continental Hotel, Lahore. I feel pleasure to invite all PFA members, casting producers, machinery manufacturers. foundry material suppliers,

service providers and global foundry technologist from various countries.

Mr. Abdul Razzak Dawood, Advisor to Prime Minster on Commerce, textile, and industry will Inaugurate IFCE-2018, with the objective to prepare local foundries for export markets. The purpose of the event is technological up-gradation and skills development.

The International foundry consultants and speakers are invited from Europe, China, India. UK, Turkev and Germany, representatives from European & Asian foundry association. They will be available to meet casting producers and users to address their issues in casting, in cast source meetings. The exhibition will provide an opportunity investors, to machinery manufacturers, foundry material suppliers



service providers to showcase their products and services. **IFCE** will have foundry exhibition and Workshops technology and Seminars for two days. They will be conducted by International foundry experts/ consultants and speakers. All foundrymen, engineers and their technical staff

from various industrial sectors are invited.

Around 25 Technical sessions of one to two hours each, have been planned during two days. Length of session depends on importance of the subject. Translators in local language will be available in each session to ensure maximum understanding of the subject. Pakistan Foundry Association team has proposed these topics for the technical session, but the experts may choice presentation according to the need of the audience.

I pray to almighty Allah for the great success of IFCE-2018 to make it a memorable event.

Sikandar Mustafa Khan President-PFA

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## State of the U.S. **Cupola Industry**

Cupola melting systems in the U.S. produce a majority of iron castings, and advancements in the melting technology has made their use sustainable into the future. david kasun, p.e., kuttner IIc (port washington, wisconsin)

Since the advent of time, cupola furnaces have melted the vast majority of cast iron worldwide and in the U.S. While the number of operating cupolas in the U.S. has decreased from about 200 to 42 cupolas since the turn of the century, advances in cupola technologies, increases in cupola efficiency and the metallurgical and cost benefits of cupolas have ensured they remain as a significant, and leading technology for iron production. The 42 cupola foundries in the U.S. produce approximately 53% of all domestic cast iron. Nearly 62% (3.75 million tons per year) of all gray iron production and nearly 38% (2.3 million tons per year) of all ductile iron production is produced by cupola melting.

Projections from AFS Metalcasting Forecast & Trends show that total annual shipments for iron castings is 6.74 million tons per year. By applying typical yield rates for the various (ductile SIC codes pipe, municipal. agricultural, automotive, etc.), estimates show that total tons melted for all iron types totals about 11.45 million tons per year. By applying knowledge-based estimates of the cupola industry, it is estimated that of the total iron melted, about 6.07 million tons per year are melted by 23 companies using cupolas.

There are SIC sectors, such as ductile iron production pipe and high automotive/industrial/municipal foundries, where cupolas are the mainstay. In other SIC sectors, demand for a wide variety of metallurgical grades have made the cupola less attractive. Cupolas have, however, remained highly competitive,

due to their flexibility, giving them a competitive advantage over electric melting methods. While cupolas are a big part of the iron melting picture in the U.S., the landscape the cupola has changed. Stricter environmental regulations in the last three decades, combined with the changing metallurgical demands in foundries, have led many to believe that cupolas are going away. While it is true that there are fewer cupolas, it can be said with certainty they are not going away anytime soon. Cupolas continue to have some advantages, compared to electric melting, but there are six primary myths about cupolas that should be dispelled.

## Myth 1: Cupolas are going away.

Many old, inefficient, obsolete cupolas have mostly gone away. While some cupolas are challenged by operation at low production rates, the remaining cupolas mostly have increased thermal efficiencies and many have incredibly high efficiency rates. Some technical advances can be made with minimal capital expenditure. The post combustion heat recovery systems are better, and cupola shops are pursuing methods to reclaim waste heat and increase hot blast temperatures (up to 1,150F) to decrease coke rates while many have found ways to beneficially reuse slag. Alternative carbon and fuel sources have been established and chemistry transition practices have been modernized. The bottom line is cupolas now are more efficient with higher productivity per unit. Many cupola shops continue to invest in technical improvements in furnace efficiency and heat recovery systems as part of their long term strategy for sustainability.

## Myth 2: Cupolas are economically infeasible.

Continuous production rates and flexibility in scrap input gives cupolas an economic advantage. Production rates are steady and predictable. A wide range of scrap input can be handled, such as dirt, high zinc, shredder contaminants, bundles, iron briquettes, high oxide content and self-reducing briquettes. In desulfurization for ductile compacted graphite base iron allows for the melting of low-cost high sulfur scrap. Cupolas can accommodate up to seven iron chemistry changes per day, supplemented with in-spout alloy additions. Cupolas are well known to have lower labor cost per unit of iron, especially for high production cupolas, say above 20-25 tons per hour.

Cupolas continue to have some advantages, but six primary myths about cupolas should be dispelled.

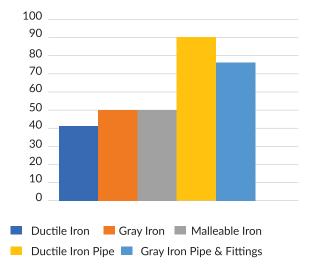
## Myth 3: It is impossible to obtain permits for cupolas.

While regionally designated environmental areas can make permitting difficult for any new foundry, new cupolas can be permitted and meet the strictest requirements. New gas combustion and dust collection technologies can meet MACT particulate matter and hazardous air pollutant and volatile organic compound standards. Gas concentrations like SOx and NOx are generally not of great concern, even in some EPA designated ozone non-attainment areas. State of the art pollution controls for cupolas have been in place in Europe for two decades, where regulations are more strict than in the U.S., proving that properly designed air pollution control systems make cupolas viable. In fact, properly designed control systems provide ultra low maintenance costs, with extended

filter life (bag changes) on the order of 8-10 years.

### **Cupolas** Myth 4: are energy intensive and inefficient.

Cupolas are inefficient only if they are following "old" methods and designs. The high efficiency cupola plants of today produce iron that is 15% less energy intensive produced from coalproduced than iron (medium electricity frequency). methods for waste heat reclamation are installed (cupola flue gases), cupolas are 40-60% more energy effective than electric melting. As electricity prices and natural gas prices increase in the future, the benefits of cupola melting, using coke as a the heat source, will become more attractive. We



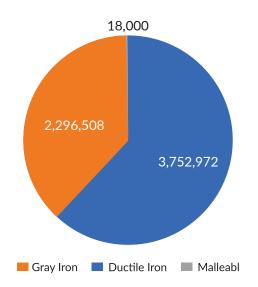
By applying typical yields to attain tons melted (corrected by SIC code sectors), it was determined that while 6.74 million tons of iron castings are shipped per year, the actual tonnage melted per year is more than 11 million tons.

should remember that only about 85% of the coke charged into a cupola is burned for heat, and that about 15% of the coke is dissolved into the cast iron as metallurgical alloy, a very effective means of arburizing iron, especially for high steel charge mixes. Technology advances extend beyond the furnace, to further to reduce the energy intensity of the entire cupola plant. Approximately 20 U.S. states have now defined industrial process

waste heat as a renewable resource, making it, in some cases, not only recognized as a resource for harvest, but also making the capital investment eligible for funding and/or tax credits. The best, most efficient cupola shops have already installed, or are actively pursuing the installation of waste heat capture systems that can harvest and re-use the heat for a variety of processes. These include:

- Plant and office makeup air heating.
- Cupola blast air dehumidification.
- Core oven heating.
- Electric power generation.
- Domestic water heating.
- Other process heating.

Investment in these technologies will significantly reduce the electric and/or natural gas consumption of the foundry and reduce the overall energy intensity of the final product, iron castings.



Shown is the breakdown of cupola production as a percent of total melted domestic tons.

## Myth 5: Coke is too expensive.

It is true that coke is somewhat costly, but prices have significantly dropped and stabilized in the last five to eight years. Electricity prices, meanwhile, have increased and been somewhat unpredictable. It appears that high quality European coke and formed coke suppliers have been placing pressure on domestic coke pricing.

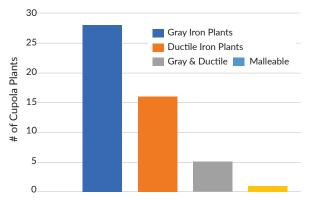
## Myth 6: Coke is not going to be available in the future.

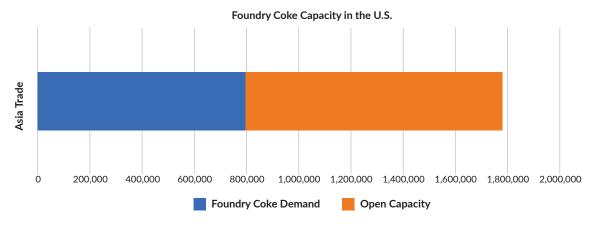
According to David C. Ailor, president, American Coke and Coal Chemicals Institute (ACCCI), the present foundry coke demand is only 38.2% of the four domestic merchant member coke-producers' capacity. Like cupolas, domestic producers are fewer, but they are strategically suited for the long-term supply of the foundry industry. The merchant coke production capacity is 1.78 million tons, while the current domestic demand is about 0.8 million tons. The four merchant members producing foundry coke have taken several steps to continue as sustainable partners for U.S. metalcasters by:

- Tailoring operations to meet the coke requirements/needs.
- Organizing to engage regulatory agencies as the need arises.
- Using many different coal blends.
- Tailoring transportation/delivery infrastructure to meet customer needs.
- Maintaining batteries to ensure long-term, reliable battery operation, performance and environmental compliance.

### U.S. CUPOLA LANDSCAPE

Forty-two cupola plants operate in the U.S., represented by 23 companies. The top 10 cupola foundries melt a combined 4,181,800 tons per year, which is 63.2% of total cupola production and 36.5% of total cast iron production in the U.S. The chart here shows the breakdown of cupola plants by metal melted.





The U.S. coke plants producing foundry coke have enough open capacity to handle double the current domestic demand. The majority of foundry coke is supplied by four merchant produceers of metallurgical coke.

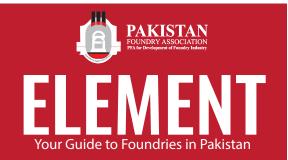
## What does the future hold?

Cupolas continue to produce the majority of iron in the U.S., especially gray iron. The benefits of modern cupola melting systems include:

- The ability for in-stream desulfurization for ductile and compacted graphite iron.
- Flexibility in alloying (charge or in-stream).
- Improvements in heat reclamation and heat recovery.
- Low labor cost.
- Low scrap cost.
- Flexibility in scrap material selection.

It is clear that "old" cupola technology will not work in the foreseeable future, especially as the U.S. sees continued competition globally. Many U.S. foundries still use methods and equipment that has been surpassed by competitors in Europe, Asia and - South America. Without the necessary investment, U.S. cupola foundries could fall behind. But it is also clear, that those foundries who continually advance their cupola technologies and improve energy efficiency. will realize a strong, competitive and sustainable means of cupola melting, well into the future.

This article is adapted from AFS Melting Methods & Material Division panel (18-122) with presentations by David Kasun and David Ailor, at the 2018 AFS Metalcasting Congress.



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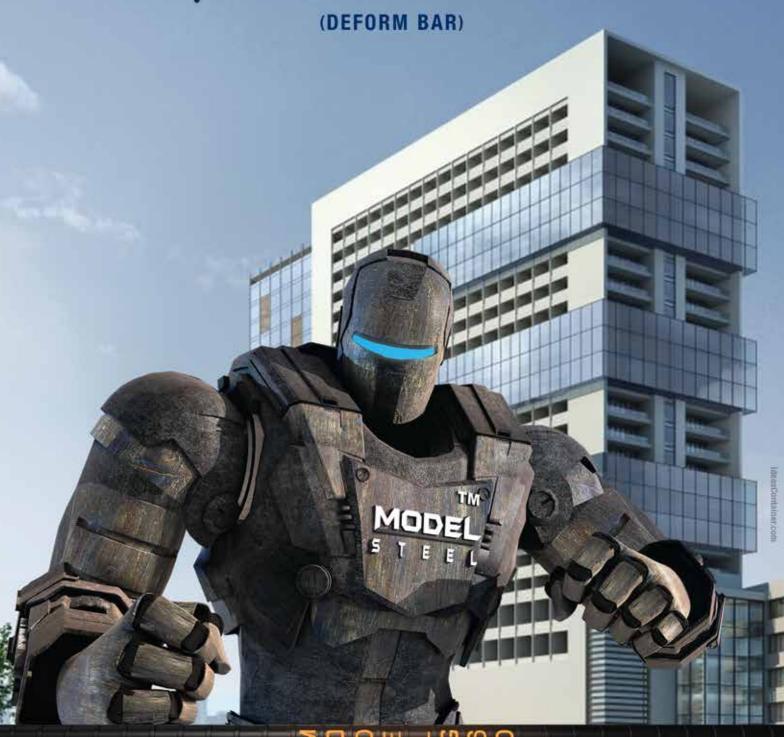


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## Marketing and Exports of Quality Castings and **Modern Technology**

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## Introduction

Marketing strategy is а long-term, forward-looking approach to planning with the fundamental goal achieving and a sustainable competitive advantage. Strategic planning involves an analysis of company's strategic initial situation prior to the formulation, evaluation and selection of market-oriented competitive position that contributes to the company's goals and marketing objectives. Marketing strategy highlights the role of marketing as a link between the organisation and its customers. At its most basic level, strategic marketing addresses three deceptively simple questions:

- (1) Where are we now?
- (2) Where are we going?
- (3) How are we going to get there?

In attempting to answer these questions, strategic planners require sophisticated skills in both research and analysis of global market for all types of quality castings.

Definitions of marketing strategy- Scholars continue to debate the precise meaning of marketing strategy. Consequently, literature offers many different definitions. On close examination, however, these definitions appear to centre on the notion that strategy refers to a broad statement of what is to be achieved.

### Marketing management versus marketing strategy

The distinction between "strategic" and "managerial" marketing is used to distinguish "two phases having different goals and based on different conceptual tools. Strategic marketing concerns the choice of policies aiming at improving the competitive position of the firm, taking account of challenges and opportunities proposed by the competitive environment. On the other hand, managerial marketing is focused on the implementation of specific targets.

## CDI and BDI

CDI means Category Development Index while BDI denotes Brand Development Index. The category/brand development index is a method used to assess the sales potential of a region or market and identify market segments that can be developed (i.e. high CDI and high BDI). In addition, it may be used to identify markets where the category or brand is under-performing and may signal underlying marketing problems such as poor distribution (i.e. high CDI and low BDI).

### BDI and CDI are calculated as follows:

BDI = (Brand Sales (%) in Market A/ Population (%) in Market A) X 100 CDI = (Category Sales (%) in Market/ Population (%) in Market A) X 100

## **Brief Description of PEST Analysis**

analysis: variables that may be considered in the environmental scan



Fig 1: PEST Analysis

Strategic planning typically begins with a scan of the business environment, both internal and external, this includes understanding strategic constraints. An understanding of the external operating environment, including political, economic, social and technological which includes demographic and cultural aspects, is necessary for the identification of business opportunities and threats. The main elements of the PEST analysis are:

- ▶ Political: political interventions with the potential to disrupt or enhance trading conditions e.g. government statutes, policies, funding or subsidies, support for specific industries, trade agreements, tax rates and fiscal policy.
- **Economic:** economic factors with the potential to affect profitability and the prices that can be charged, such as, economic trends, inflation, exchange rates, seasonality and economic cycles, consumer confidence, consumer purchasing power and discretionary incomes.
- **Social:** social factors that affect demand products and services, consumer preferences attitudes. tastes and like demographics, social influencers, role models, shopping habits.

**Technological:** Innovation, technological developments or breakthroughs that create opportunities for new products, improved production processes or new ways of transacting business e.g. new materials, new ingredients, new machinery, new packaging solutions. new software and new intermediaries.

## Relationship between marketing strategy and marketing policy

The generic, competitive strategy provides overall structure and guidance for day-to-day operational planning and decision-making. The 4P's are very important which can be considered as under -

- Price
- Product
- Place and
- Promotion

This is also known as the marketing mix or marketing programme representing the tools that marketers can use in day-to-day operational planning. This marketing programme enables marketers a means for turning the long-term vision into every day practice. Similarly SWOT analysis is also significant in marketing of castings.

In addition to the PEST analysis, firms carry out a Strengths, Weakness, Opportunities and Threats (SWOT) analysis. A SWOT analysis identifies:

- Strengths: capabilities. distinctive competencies, skills or assets that provide a business or project with an advantage over potential rivals; internal factors that are favourable to achieving company objectives
- ▶ Weaknesses: internal deficiencies that place the business or project at a disadvantage relative to rivals; or deficiencies that prevent an entity from moving in a new direction or acting on opportunities. internal factors that are unfavourable to achieving company objectives

- ▶ **Opportunities:** elements in the environment that the business or project could exploit to its advantage
- ▶ **Threats:** elements in the environment that could erode the firm's market position; external factors that prevent or hinder an entity from moving in a desired direction or achieving its goals.

Typically the firm will attempt to leverage those opportunities that can be matched with internal strengths; that is to say the firm has a capability in any area where strengths are matched with external opportunities. It may need to build capability if it wishes to leverage opportunities in areas of weakness. An area of weakness that is matched with an external threat represents a vulnerability, and the firm may need to develop contingency plans.

### Market-based resources include:

- ▶ Organisational culture e.g. market orientation, research orientation, culture of innovation, etc.
- Assets e.g. brands, Mktg IS, databases, etc.
- ► Capabilities (or competencies) e.g. market sensing, marketing research, relationships, know-how, tacit knowledge, etc
- Some marketing Managers suggest the following classification of competitive positions:
- Price positioning
- Quality positioning
- Innovation positioning
- Service positioning
- Benefit positioning
- Tailored positioning (one-to-one marketing)

Four Squares of Time management is also very significant for marketing of castings (Fig 2).

## Time management matrix



Fig 2:Time Management matrix

Till now the important parameters of good marketing strategies have been considered. Many foundrymen from India from time to time attend international exhibitions and Congresses/conferences in foreign countries like GIFA, Hannover Fare, Metal China, World Foundry Congress, World Technical Fourm etc and exposed to new innovative and advanced technologies. They should apply these production techniques in their foundries to ensure that they can produce quality castings of ferrous or non-ferrous castings for export.

### **Export of Indian castings to global market**

However, the Indian aluminium Gravity and High Pressure Die castings have good global market particularly for space craft internationally. These castings are produced particularly by Investment Casting Process (Fig 3).

India is in number two just after China in world ranking of casting production. China is producing castings in large volume however, the quality of Indian castings is far better than that of China.



Fig 3: Number of Investment Casting foundries worldwide

This means Indian foundries cannot produce large number of castings per month for exporting just because the foundries have limitation due to the capacity of production as the limited machines available in all sections of foundries. Therefore, they cannot compete with their Chinese counterparts.

## **Market Prospects**

HPDC Casting are mainly consumed all over the world by

- 1. Automobile Industry
- 2. Electrical & Electronic Industry
- 3. Communication Industry (Mobile Phones, Laptop Bodies , etc)

Market prospects of HPDC processed castings

## Export of Indian castings of all types of ferrous metals

Table-1: Production castings and energy consumption

Type of casting Produced	Melting Technology	Specific Energy Consumption (MJ/KG)			
		Min	Average	Max	
Cast Iron	Induction furnace	3.57	3.78	4.05	
	Cupola	3.05	3.79	4.86	
SG Iron	Induction Furnace	4.50	4.91	5.32	
Steel	Induction Furnace	4.50	4.74	5.22	
Cast Iron and SG Iron (hybird units)	Induction Furnace	-	3.66	-	

The above table shows all types of cast iron castings are exported globally.

So, what innovative technology is for Indian foundries. For example, there is no foundry producing compacted graphite cast iron (CGI). This is a patented process by Sintercast Pvt Ltd, UK and Dr Steve Dawson is the President & CEO of this company. He is very helpful to Indian Foundries however, many foundries consider that the cost of producing CGI in this process very expensive so they are less interested in going for this technology. There are a number of foundry clusters which are producing ferrous and non-ferrous castings as per international standards and exporting castings to various destinations across the globe (Fig 4).



Fig 4: Foundry Clusters in India

In the latter part of this article quality aspect of castings with relation to marketing and export of the same at competitive cost has been discussed. New concepts of production technology are coming in from countries like Japan, Germany etc. "Nodularity" in aluminium-silicon alloys and substitution of steel castings by Ductile Iron may be mentioned in this respect. Some problems faced by some overseas foundries and solutions thereto have been covered in the following case studies.

These are (1) "IDAS" in aluminium alloys (2) "Nodularity" in aluminium alloys (3) "WHN" Hardness Testing and (4) "Replacing Steel Casting" by ferritic ductile iron.

## Case Study - 1

IDAS in Aluminium alloys microstructure measurement

Measurement of Inter Dendritic Spacing (IDAS):

The most commonly casting alloys are of hypoeutectic type. It contains dendrites of alpha in a matrix of eutectic which is in inter dendritic spacin. The measurement of this Inter Dendritic Arm Spacing (IDAS) has effect on the properties of castings. There was a difference in difference of opinion between German and Indian experts in respect of the methods of measurement of IDAS in microstructure.

Microstructure of hypo-eutectic Al-Si alloy:

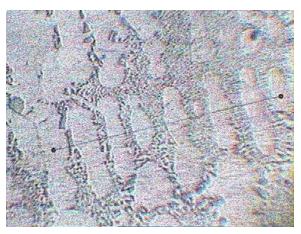


Fig 5: German Method of measuring IDAS

German Method - They draw a line through the dendrites and measure the length of the line in microns and divide the total number of alpha dendrites to get SDAS in microns at 200X magnification.

Total length of line 473 microns/7 dendrite = 67.50 microns

Indian method of measuring IDAS:





Fig 6: Indian method of IDAS measurement

Same Number of dendrites was selected and measurement of width of eutectic spacing was carried out. Average of that was reported which was between 13.3 to 20.0 microns as compared to German method which was 67.50 microns. It was demonstrated on different specimens.

- (A) Readings of IDAS were 11, 20, 16, 25, 43, 25, 16 and average of 20 microns at 200 X magnification.
- (B) Readings of IDAS were 20, 15, 12, 09, 13, 15, 13 = 97/7= 13.38 microns at 200 X magnification.

## Case Study - 2

## Concept of nodularity in aluminium-silicon alloys

The term "nodularity" in ductile iron is well known. Now Japanese specifications for aluminium-silicon alloys include concept of "nodularity" of the alloys. It is sometimes confusing but they have clarified that the "nodularity" of alloys indicates the efficiency of modification treatment given to liquid metals. It is simple that modification treatment is given to convert the silicon phase in eutectic shows to spherical form just like nodules in ductile iron. This can be accurately measured under microscope. Higher the nodularity better is the ductility of the alloy.

Nodularity of any grade of ductile iron for different components is quite common. That entirely depends on controlled by the composition of the molten metal during melting. It also depends on the magnesium treatment to be given in treatment ladle. The pouring techniques are also have effect on the nodule count and the properties of castings. Thus the new concepts can be solved by proper study of Metallurgical of that alloy during melting and metal treatment. In addition, the complete solidification of that alloy casting in moulding must be understood.

## Modern Techniques of Metallography

Histogram showing even distribution of eutectic nodules (Fig 7 & 8).

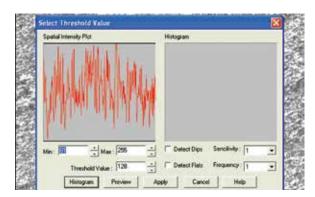


Fig 7: Histogram showing distribution of eutectic nodules

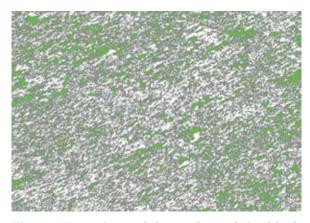


Fig 8: Eutectic nodules coloured in black small nodules

## **Observations and conclusions**

From indepth metallurgical examination and the new techniques used for microstructure observations it is clear from the Histogram that the eutectic structure is well-modified throughout and nodularity of eutectic shows that the modification treatment given was very perfect and useful to improve the mechanical properties of the alloy. Nodules of eutectic will improve toughness of the aluminium-silicon alloy.

## Case Study - 3

## WHN Measured on Normal Hardness Testing Machine

The term 'WHN' is used to measure hardness of very hard castings that are wear resistant. The BHN hardness testing machine can be used for WHN but the diameter of ball used is 10 mm. Load is also 3000 lbs. However, the ball used must be made of Tungsten Carbide. Tungsten is denoted by W, so it is called WHN.

Normally, WHN is related to hardness Rockwell Rc and not BHN.

Normally BHN is used for soft metals while Rockwell harnesses are used as Rockwell Ra, Rb and Rc are used for slightly higher harnesses but for more hardness only Rockwell Rc is used. In all these, the indenter is different such as Ra and Rb; the indenter used is of hardened steel. It is sometimes called "Brale" indenter. Rockwell Rc is used for very hard metals. The indenter used is a square based cone. The indention of this test is square shaped. The average of two diagonals is taken for calculation of area of indentation. One more test criteria as compared with BHN is that initially 10 lbs. Load is applied so that there will not be some recovery as found in BHN.

## Case Study No 4

## Replacement of Steel Casting with Ferritic Ductile Iron DIN GGG 40 by German Company

## A case study of M/S Vulcan Technologies Pvt Ltd, Pune

Vulcan Technologies Pvt Ltd produces a variety of castings of couplings of different types. They had a typical practical working problem during working of L - shape ring and Hub steel castings when a rubber ring was fitted on the exterior outer circular surface of casting (as shown in the pictue) of "L - shape ring casting of steel" (Fig 9).



Fig 9: Shape of ring castings of steel

## **Problem**

The problem was of adherence of rubber with the surface of steel casting during working. It was thought that it could be solved if the cast material (steel) was replaced by some other material.

## Solution

The points considered for the replacement of steel by SG iron for better adherence of rubber with surface of the casting were as under.

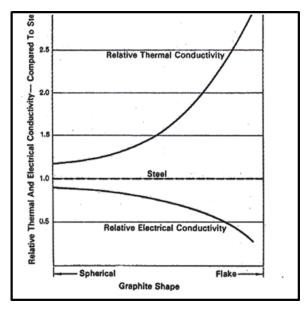


Fig 10: Effect of Graphite shape on the relative thermal and electrical conductivity of grey and SG iron as compared to steel

## Thermal conductivity of steel and cast iron

The thermal conductivity of steel or cast iron is influenced by the microstructure of steel or cast iron in discussion. The thermal conductivity of iron grey at room temperature is approximately same as other ferrous materials ranging from 0.110 to 0.137 Cal/sq cm/sec/cm/ C depending upon microstructure of the grey or SG iron.

The following table indicates the effect of micro-constituents on thermal and electrical conductivity in relation with temperature.

Micro-constituent	Thermal Conductivity at different Temperatures			
	0 - 100oC	500oC	1000oC	
Graphite	0.7 - 1.0	0.2 - 0.3	0.1 - 0.15	
Ferrite	0.17 - 0.19	0.1		
Pearlite	0.12	0.1		
Cementite	0.017			

From the above values it was clear that Ferritic SG iron (GGG40) has superior thermal conductivity as shown in the graph. The graph actually shows higher thermal conductivity of flake graphite than nodular or SG iron however, due to its lower torsion fatigue it is not recommended for our application.

- Specific gravity: The specific gravity of steel is 7.7 gm/cm3 while that of SG iron is 7.1 gm./cm3. So, there would be less weight of the castings and so less cost.
- Shrinkage tendency: Steel has higher shrinkage during solidification of casting hence higher risering is required to compensate the volumetric shrinkage in casting. In this case, due to higher yield of casting more fettling work is required increasing cost of production.
- Bonding factor with natural rubber: Normally, bonding of rubber on metallic surface of SG iron is higher due to presence of graphite nodules which act as an interface between metallic matrix and rubber. This is also because of better thermal conductivity of SG Iron compared to steel.
- Machinability of SG iron: Machinability of SG iron is better than that of steel due to presence of graphite nodules which break the continuity of metallic matrix. The chip formation during machining is segmental while in steel it is continuous ring formation that also affects the surface finish of casting after machining.

So, in conclusion it can be said that modern technologies are urgently required to be adopted for production of quality casting complying with customer specifications and exporting them to the international markets.

## References

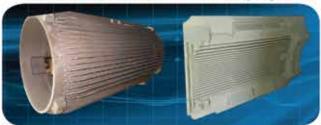
- **1.** Study of marketing strategy of our foundries by visiting foundries in India.
- **2.** Study of marketing research available in Wikipedia free in Google.
- **3.** Case studies brought to the author by his students working in various foundries and he could give them the solution. Nodularity in aluminium-silicon alloys was brought by Noblecast Pvt Ltd, Pune.
- **4.** Case study of replacing steel casting given by Vulcan Technologies Pvt Ltd Pune who have been exporting castings to German companies also.

consistent quality increased productivity wide accessibility prompt technical backup









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Phenolic urethane gassing cold box
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Furan no bake (steel, SG, CI, NF)
CO<sub>3</sub> cured phenolic
Inorganic no bake system

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Graphite spirit/water based
Alumino-silicate mix refractory spirit/water based
Magnesite spirit based
Graphite water base for metallic trough
Bismuth base coating

Coating for lost foam process Tellurium base coating

Sulphur blocking coating

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- Release agent for alkaline phenolic no bake system.
- Release agent for cold box
- Parting agent for shell (water / solvent based)
- Aluminium based release for no bake system

### Core joining paste

- Hot to hot
- Cold to cold
- Cold to cold (ultra fast)

Collapsible agent for silicate

Mould sealing rope

Sealing compound for mould and core Silicon carbide, zirconia foam filters

Ceramic sand

Chromite sand

Slag coagulant (perlite ore)

Sand Additives (Sphereox) of Chesapeake Specialty Products, USA Furnace & refractory cleansing fluxes of ASI International, USA

- Redux EF40L briquettes
- Redux EF40 bricks

Additive for thermal reclamation of alkaline phenolic no bake resin.

Anti-Veining solution from John Winter & Co., UK

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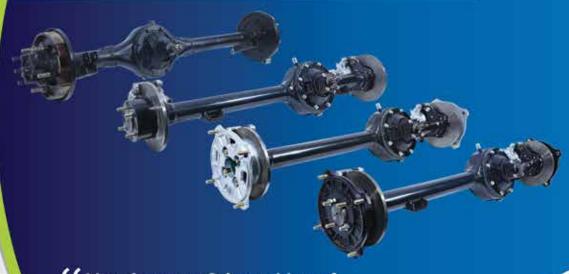












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## **Heat Treatment**

## Ir G Henderieckx Gietech BV

Heat treatment is called every, by purpose, temperature change and returning back to room temperature.

The purpose is to achieve, in castings or other parts, a target condition (mostly about residual stress), microstructure and mechanical and or physical properties.

A heat treatment is extra cost and should be avoided if possible.

This possibility is present for grey, ductile and compacted iron, although sometimes heat treating is done for correcting microstructure and carbide presence.

Materials that solidify dendritic (all steel and white solidifying iron) always need a heat treatment for getting a homogeneous structure and grain size.

There are 4 important temperatures: Ac3, Ac1, Ms and Mf (all depending on the chemistry of the material).

Ac1 is the temperature above which the austenite structure is formed.

Ac3 is the temperature above which only austenite (exception delta-ferrite) can be present.

Formula (all in °C) according Andrews:

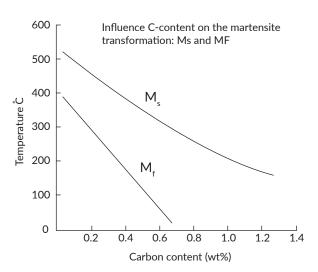
Ac3 = 910 - 203 x (%C)1/2 -15,2 x(%Ni) + 44,7 x (%Si) + 104 x (%V) + 31,5 x (%Mo) + 13,1 x (%W)

Ac1 = 723 - 10,7 x (%Mn) -16,9 x(%Ni) + 29,1 x (%Si) + 16,9 x (%Cr) + 290 x (%As) + 6,3 x (%W)

Ms is the temperature below which austenite starts transforming to martensite.

Mf is the temperature below which no austenite can be present anymore. Formula (all in °C) according Andrews:

Ms = 539 - 423 x (%C) - 30,5 x (%Mn) - 17,7 x (% Ni) - 12,5 x (% Cr) - 71,5 x (%C)x(%Mn) - 67,5 x (%C) x (%Cr)



The heat treatment exist of 3 steps: first changing the temperature; second staying at the temperature for equalizing the temperature throughout the material section and possibly have a transformation (or stress relieve); third returning to room temperature.

The heating temperature rate (except for cryogenic treatment) is important for not creating too high thermal stress that can lead to cracks (especially for complex shaped castings). The transformation will happen above Ac1-temperature and be finished above Ac3-temperature.

The dwelling time (time on temperature) has the function to equalize the temperature throughout the material section and to assure that the target transformation (getting complete austenite structure, dissolving carbides...) is finished.

This process is ruled by the temperature (difference between the temperature and the Ac3-temperature) and time on temperature. The old rule of 1 hour plus 1 hour per 25 mm is obsolete and sometimes negative. Mostly

0,5 hour plus 0,5 hour per 25 mm is proven to be sufficient.

Once the austenite is formed, during all the dwelling time, the grain size will increase. This is mostly not preferred because large grains decrease the yield strength and mostly increase the brittleness.

The cooling (except for cryogenic treatment) is the phase where the new microstructure is set and the carbides are appearing or not. It is the most important step of the heat treatment. It is also important for the stress in the treated casting. The stress that will be the combination of the physical stress (difference in shrinking), the transformation stress (especially for martensite) and the thermal stress (due to temperature difference in casting sections).

The cooling can be in calm or forced air, oil, water, gas or copolymers, all of them having a particular cooling rate.

WATER COOLING SECTION WITH DIAMETER

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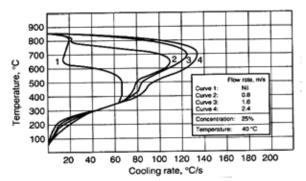
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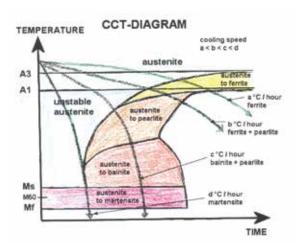
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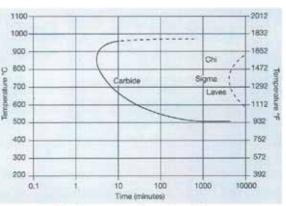
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QUENCHANT: POLYMER CONCENTRATION: 25 % TEMPERATURE: 40 °C

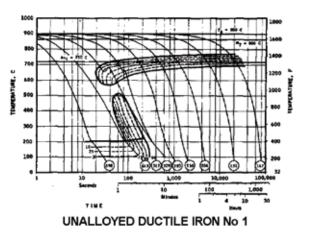


Agitation Curve 1 Nil Curve 2 0,8 m/s Curve 3 1,6 Curve 4 2,4 m/s The CCT diagrams will predict the microstructure, presence of carbides (especially for austenitic material) and the hardness. Next figures are giving the principle, example for steel, austenitic steel and ductile iron.





Carbide & secundary phases formation Stainless steel 316



## Remarks:

- 1. No heat treatment will change the free graphite!
- 2. The maximum hardness of quenched material is depending on the C-content. The alloying elements have an influence on the hardenability (difference in hardness between the surface and core of the material section).

## **Common Types of Heat Treatment**

## 1. Normalizing

Heating the material above Ac3-temperature (austenite zone) and cooling in calm air.

Homogenizing the microstructure (removing dendritic structure) and grain size.

All steels (except austenitic steels) will have this treatment after cooling from pouring.

## 2. Annealing

Heating the material above Ac3-temperature (austenite zone) and cooling in a way to get the lowest hardness.

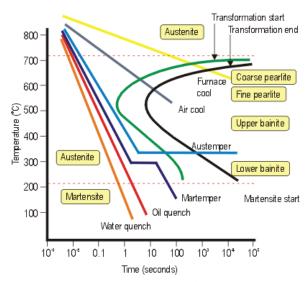
Heating the material just below the Ac1-temperature (austenite zone) and cooling in a way to get the lowest hardness.

Homogenizing the microstructure (removing dendritic structure) and grain size as well as removing the carbides in order to get a low hardness.

Applied for steel and iron castings.

## 3. Quench & Tempering

Heating the material above Ac3-temperature (austenite zone) and cooling in a way to get the required microstructure and hardness. There is always a tempering treatment of which the temperature depends on the as quenched hardness and the target hardness. The tempering will restore the ductility, especially in case of martensitic structure.



## CCT DIAGRAM

Homogenizing the microstructure (removing dendritic structure) and grain size as well as getting a high strength and hardness, combined with a fairly ductility.

Applied for alloyed steels and sometimes alloyed iron material.

In case of austenitic iron and steel, to avoid the formation of carbides.

Special hardening effect after quenching are present if the Mf-temperature is below room temperature:

- 1. heating till bainite zone for transforming the residual austenite to bainite
- 2. cooling to a temperature below the Mf-temperature for transforming the residual austenite to martensite.

It is preferred, in both cases, to do a second tempering treatment.

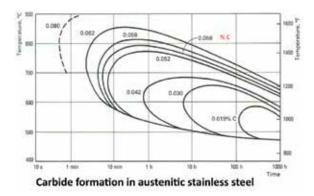
## 4. Stress Relieving

Heat treatment for removing the stress introduced during the cooling of the casting (after pouring or sometimes heat treatment). This treatment has never a microstructure change and will not influence the mechanical properties.

The stress is the sum of the thermal stress and the transformation stress.

Stress relieving is also done after welding, intensive fettling and or machining, especially for parts that must have a close dimensional tolerance

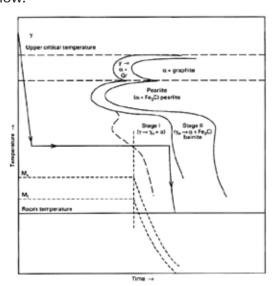
Stress relieving of austenitic material is very difficult because at temperatures above 550 °C will give way to carbide formation.



## 5. Austempering

Heating the material above the Ac3-temperature, transformation to austenite completed, then quick cooling to a temperature at which bainite is formed, holding that temperature until the austenite is completely transformed to bainite, after that cooling to room temperature.

The bainite structure is a high strength (medium hardness) structure with a high ductility. The necessity for a tempering is very low.

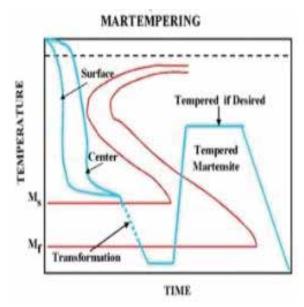


Applied to alloyed steel and ADI ductile iron.

## 6. Martempering

Heating the material above the transformation Ac3-temperature, to austenite completed, then quick cooling to a temperature at just above Ms-temperature, holding that temperature until the complete material section is at the same temperature (and bainite not yet formed), after that cooling to room temperature. During this cooling martensite is formed.

This treatment leads to a low stress level and lower risk for cracking and deformation. The necessity for a tempering is low.



Applied to alloyed steels.

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## **Concept of Neutral** Refractory lining in **Coreless Induction Furnace**

Jaydip Goswami\*, Bismit Ghosh, Sandip Samaddar , Vidosh Sarup , Virinder Khosla Saint - Gobain, Grindwell Norton Limited, Performance Ceramic Refractories, India

## Abstract

A coreless induction furnace consists of a refractory nonconductive crucible. surrounded by a coil of copper tubes. Running a powerful alternating current through the coil creates a magnetic field that induces electric currents inside the metal and quickly melts the charge inside the furnace. Proper and well -maintained refractory linings are important for a safe operation of the induction furnace.

Choosing the right refractory material for a given melting or holding application is important. Neutral Ramming Mass (NRM) has superior performance, longer life etc over conventional Silica or magnesite ramming mass.

## Introduction

Important parameters for designing a NRM are selection of raw materials & Binders, Granulometry, Density, Thermal expansion, Fired Strength, Refractoriness, vitrification temperature and resistance to chemical attack. Refractoriness must be sufficiently high so that the mass will not melt at high temperature.

There is a situ spinel formation (MgO.Al203.)

at steel melting temperature for NRM refractory.

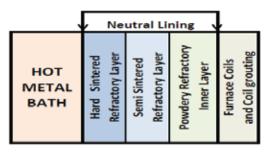


Fig 1: Schematic diagram of multi-layer concept of NRM.

## CDI and BDI

NRM is the main working lining and designed in the concept of in situ Spinelisation which associated with:

- a. Volume expansion and provide rigid structure.
- b. Hard sintered refractory surface layer resistance to metal bath and erosion.
- c. The inner refractory layer will be in powdery form.
- d. As soon as the top layer eroded, the next inner layer exposed to the metal bath and become sinter by in situ spinel formation.

## Discussion

Sintered layer is in direct conatct with Hot Metal and Slag This layer actually undergo interactions between Slag and the Refractory lining at working Temp . This Black sintered layer actually prevent slag penetration. Black sintered layer thickness should be hard & thin . This is a crtical parameter as a resistance to slag attack and longer life . Higher the black sintered thickness ,indicates more erosion in lining due to Slag – Refractory reaction and furnace life will be lower. Refractory used should be very pure and withstand the severe slag attack at working temp.

Semi-Sintered layer is the next inner layer . This is not in direct contact with hot metal & slag and remained unaffected by direct Slag attack. This is softer than sintered layer and white in color . During operation , when sintered layer gradually eroded, next inner semi-sintered layer become harder and form sintered layer. Temparature profile will be lower at the back of the lining . Semi-Sintered layer actually interface between Sintered and Powder layer and protect the lining from damage by sharp object like heavy scrap etc. If Semi-sintered layer not there, then in case of any damage of sintered layer, Powder start fall and lining may collapse. Generally thickness of White colored Semi-sintered layer higher than Black Sintered layer.

Powder layer is available at extreme back up i.e near to coil coat and reqd for multiple Patching cycle.

The thickness of Sintered – Semi-sintered – Powder layer thickness varying at different zone of the same furnace depending the working temp and metal contact time . Generally at Furnace Top portion , total remaining lining thickenss higher ( due to less erosion and less metal contact ) and the thickness will be lower at furnace center and bottom , due to more expose to working Temp / higher metal & aggresive slag contact . Again , this pattern varying from furnace to furnace and also depends on charge mix , operation parameter. Depending on the various application ,forma design to be done

to have the optimum lining thickness to get the best performance.



Fig 2: Metal contact sintered layer of NRM

Saint -Gobain has specially designed NRM (VA1248LG ) for bigger induction furnaces. This is a fused alumina based dry vibrating refractory. Due to the presence of Fused grains, compact grain size distribution and spinel bond, it is highly resistance to slag attack. It is a high purity system, using very high purity raw materials in aggregate and matrix, i.e. very low content of impurity and fluxing material . This restrict to form low melting liquid phases during operation and the dense hot face is highly resistance to erosion. The bigger grains presence provide excellent resistance to hot metal abrasion, erosion, stress and thermal shock during operation and increase the direct life. Selective use of binders & additives provides, less sintered layer thickness supported by more back up powder layer.

The sintered layer can be easily cheap out before patching and back up powder layer can be utilized for next patching cycle. Due to its excellent resistance to slag attack & erosion

Resistance, the metal contact sintered black layer thickness will be less. This indicates very dense hot face with no saturation at all and good semi-sintered & non-sintered back up.

A proper installation is as important to the safe furnace operation as the selection of the right refractory material. If the refractory material is inadequately compacted, voids or low density areas may create weak spots easily attacked by the molten metal.

The sintering procedure provided by the refractory manufacturer must be followed and never hurried. If the refractory material is not given enough time for proper bond development, the lining will be prone to attack by molten metal and slag. The sintering schedule must be completed once it has started. Chemical erosion depends on porosity level, slag chemistry and presence of high oxidation potential constituents like FeO, SiO2, MnO, Cr203, too high slag fluidity, unsaturated slag in MgO, long operating time at high temperature. Because of the above parameters, infiltrated slag weakens the refractory matrix bond and causes erosion. Different stresses associated during furnace operation like Mechanical stress ,Thermal shock ,Hot Metal Abrasion,Hot metal erosion . Particularly in Bigger Furnace, all the stresses are very high and lining eroded fast as a cumulative effect of all stresses.

One of the main weaknesses of conventional silica refractory is the formation of low-temperature melting corrosion products, causing severe and rapid erosion. The high-alumina refractories have refractoriness, no low temperature liquid formation with slag, and better corrosion resistance.

## Case - Study

This is a comparative cost sheet and case study in 12 MT Induction Furnace (Silica vs Neutral lining) in Pakistan Rs.

est Payameter	Silications	plica side/Patch	Neutral Eining	Neutral patching
lamming matrial consumption per lining-Furnace size-12 ton)	3400	9000	\$500	12500
to of settling		3	2000	5
		27	55	276
log Lining life	12	12	18	12.5
urnace output in Tons	108		795	1427 5
ing Production (in tons)(Life + furnace output)	211	324		
amoning material (anded cost —(Rs/tox))	1800	8800	205000	305000
opping material (unded cost — Po/tox)	_		_	
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ormer cost			12000	60000
etal cost in Rs.	30530	84000	1141100	2680500
Cost/int	292	250	1596	765
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haduction in one campaign of 130 heatsin tons	3960.00		4152.50	
aving of Fixed expenses on extra production @ Fix 15-00/fron			268750:00	
inst saving in neutral Lining due to extra production (Rs./ton)			69.54	
verses faver in twh	645.00		639.00	
rower (12 unit/hori) @Rs.34/unit) in Neutral Lining			288	
inn Consumption				
item Saving @ 1.7/Agiton, Simm cost Fo 216/Ag in Neutral lining			357	
			111.50	
etal Corolina	267.61		199.76	

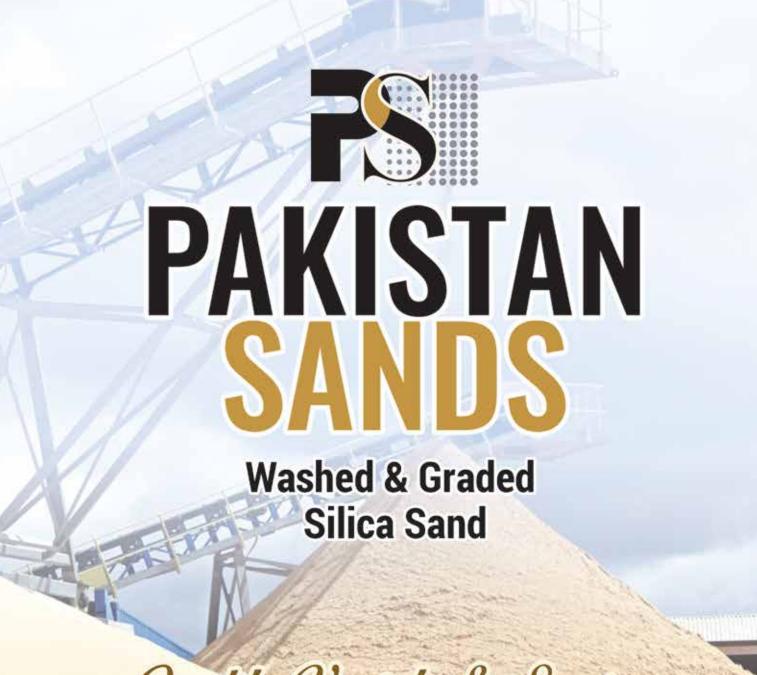
## **Conclusions**

The selection of refractory lining is a key for coreless induction furnace to reach the longest possible life with optimum cost, in current hard competition and tight market conditions. Although the initial cost of Neutral Ramming Mass is higher than silica, it is still overall profitable if we consider the costs of former and mica, labor, energy, production loss, higher metal output, etc.

Neutral Ramming Mass has 3 Phase structure - Sintered / Semi-Sintered/ Powder layer during operation, combine effect of 3 - Phase results Slag/Metal resistance, longer life . At the end of lining life, patching can be done with Neutral Ramming Mass by keeping the virgin powdery backup, so overall campaign life can be increased with Neutral.

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- [4] Ozan Uylas<sup>1</sup>,<sup>2</sup>, Muharrem Timuçin<sup>3</sup>, Ender Suvacı<sup>1</sup>, Muammer , Bilgiç5, Özdemir4, Oktay Uysal², Uğur Cengiz5, Özkan, Kurukavak4, Hasan Erdoğan4, Yakup " Mortem Study on Al2O3-MgO Induction Furnace Linings ".



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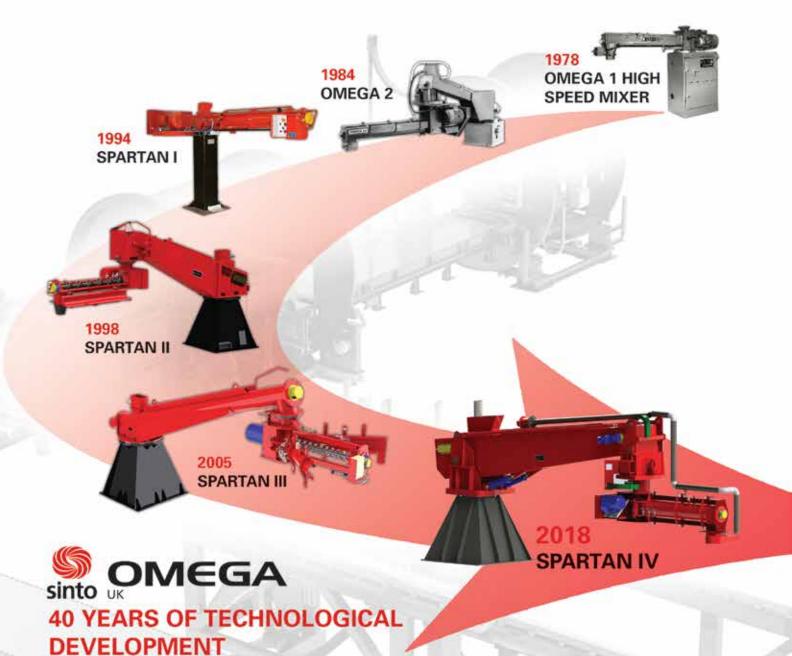
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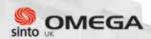
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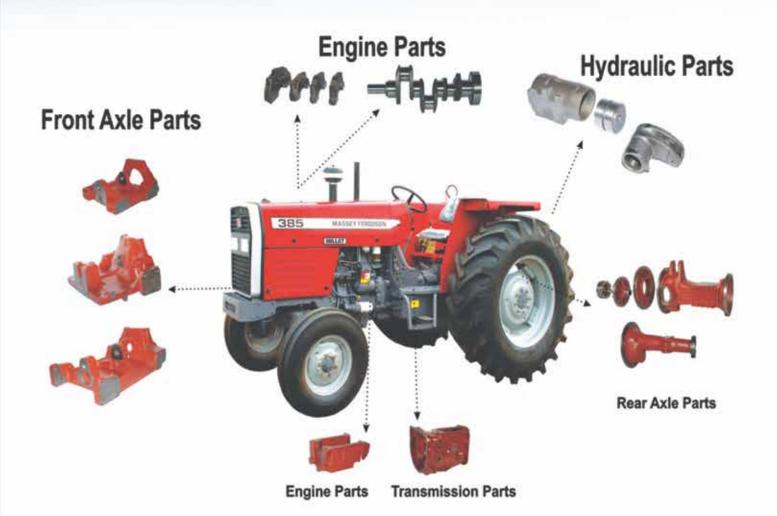






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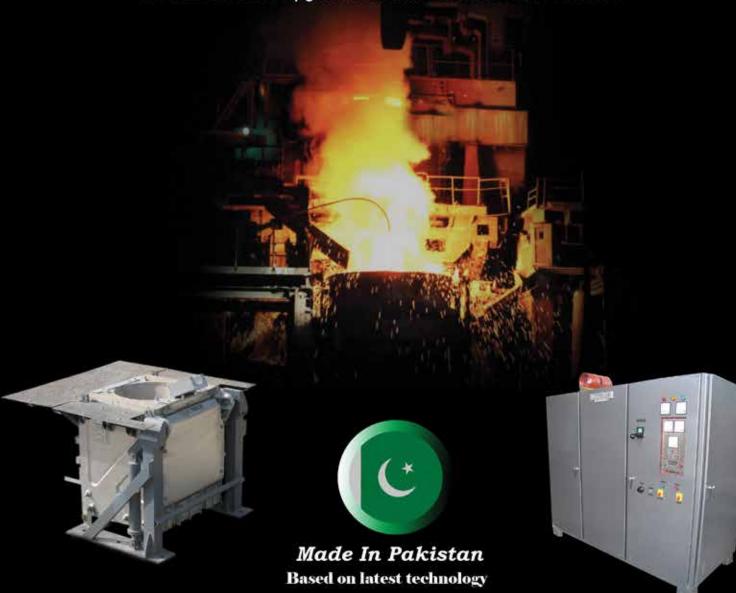
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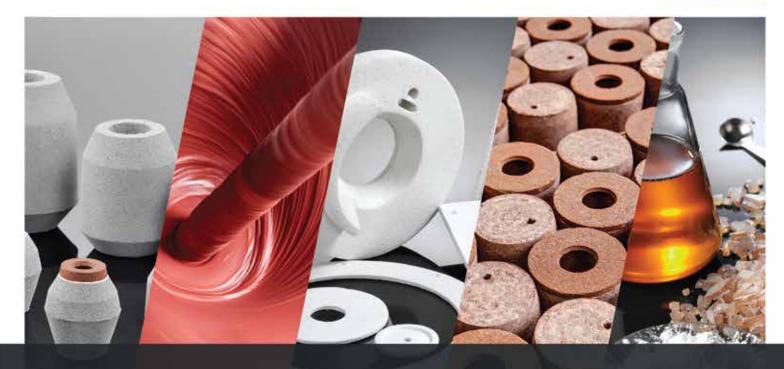
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